# Solubilities of Carbon Dioxide in Aqueous Potassium Carbonate Solutions Mixed with Physical Solvents

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The solubilities of carbon dioxide in aqueous potassium carbonate  $(K_2CO_3)$ solutions mixed with physical solvents were measured at 298.2 and 323.2 K with a CO<sub>2</sub> partial-pressure range of 5 kPa to 2 MPa. 1,2-propanediol and propylene carbonate were selected as physical solvents. The aqueous solutions treated in this study were 5 mass % K2CO3-15 mass % 1,2-propanediol, 5 mass % K<sub>2</sub>CO<sub>3</sub>-30 mass % 1,2-propanediol, 5 mass % K<sub>2</sub>CO<sub>3</sub>-7.5 mass % propylene carbonate, and 5 mass% K2CO3-15 mass% propylene carbonate. The experimental solubility results were presented by the mole ratio of CO<sub>2</sub> and K<sub>2</sub>CO<sub>3</sub> contained in the liquid mixture. The addition of 1,2-propanediol to 5 mass % K<sub>2</sub>CO<sub>3</sub> solution lowered the solubility of CO<sub>2</sub> at constant temperature and pressure conditions within the CO<sub>2</sub> partial-pressure range of 5 kPa to 2 MPa. In the case of propylene carbonate, the addition of propylene carbonate increased the experimental solubilities in the region of low CO<sub>2</sub> partial pressures and decreased as the CO<sub>2</sub> partial pressure was increased above atmospheric. The solubilities of CO<sub>2</sub> decreased with increasing temperature in the range of 298.2 to 323.2 K.

**KEY WORDS:** absorption; aqueous solutions; carbon dioxide; potassium carbonate; solubility.

# **1. INTRODUCTION**

The removal of acidic gases such as  $CO_2$ ,  $H_2S$ , and COS from gas streams is a very important operation for petrochemical, oil refineries, ammonia manufacture, coal gasification, and natural gas purification plants [1]. The common techniques for the bulk removal of carbon dioxide are based on

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chemical and/or physical absorption [2]. In physical absorption, the solubilities of gases in absorbent solutions are proportional to the partial pressures of the solubilized gases in the feed. The magnitude of the heat of absorption in physical absorption is lower than that in chemical absorption. The physical absorption process can be more advantageous in the high partial-pressure region where the treated gas removal at low partial pressure is not required. On the other hand, chemical absorption is the coupling reaction between chemical absorbent and treated gas, and the resulting solubilities are mainly governed by the stoichiometric relations. Since the capacity is not highly sensitive to the gas partial pressure, it is preferable for the case where the removal to high purity is required.

Aqueous alkanolamine and potassium carbonate solutions are known to be typical chemical absorbents used for the removal of acidic gases. The use of blended alkanolamine solutions can have a combination of the merits of amines such as higher loading capacity and faster reaction rate [3]. In addition, mixed solutions of amines and physical absorbents such as sulfolane [4, 5], propylene carbonate, N-methylpyrrolidone [6], and methanol [7] can improve gas solubility at high-pressure conditions and save the energy requirements in the regeneration step. In particular, aqueous potassium carbonate solutions are commonly used in hot carbonate processes for bulk CO<sub>2</sub> removal because of their low cost, large capacity, ease of handling, and relative ease of regeneration [1]. Although several studies have been reported in the literature [8-10] for solubilities of acidic gases in K<sub>2</sub>CO<sub>3</sub> solutions, they are mainly focused on the relatively high concentration range of  $K_2CO_3$  at high temperature conditions. In our previous study [11], solubilities of CO<sub>2</sub> in aqueous K<sub>2</sub>CO<sub>3</sub> solutions at low concentrations of  $K_2CO_3$  and moderate temperatures were measured.

On the other hand, the present study covers the solubilities of  $CO_2$  in aqueous  $K_2CO_3$  solutions and  $K_2CO_3$  solutions mixed with 1,2propanediol and propylene carbonate at 298.2 and 333.2 K which were measured in the  $CO_2$  partial-pressure range of 5 kPa to 2 MPa. The objective of this study is to measure the equilibrium solubilities of  $CO_2$  at various combinations of the liquid absorbents and to investigate the effect of the physical absorbents on the solubilities by comparing with the results when only  $K_2CO_3$  is used.

# 2. EXPERIMENTAL

#### 2.1. Apparatus and Procedure

The equipment and procedure used for the solubility measurements are the same as for our previous investigation [11]. The main apparatus consists of an equilibrium cell, sampling compartment, and gas chromatograph. The equilibrium cell is made of 316 stainless steel with an internal volume of about 400 cm<sup>3</sup>. A vapor sampling valve (Rheodyne, 7410) with a loop of about 500  $\mu$ l was connected to the gas chromatograph (Young In, M600D) equipped with a thermal-conductivity detector (TCD) for the on-line measurement of the vapor sample. The column is 1.83 m length by 0.0032 m diameter and packed with Porapak Q. Most components of the apparatus are contained in a water bath except the gas circulation lines. To keep the temperature uniform in the apparatus, the lines exposed to room temperature were enclosed by heating coils.

To begin an experiment, an aqueous solution of about 250 ml was added to the equilibrium cell, and all the lines were purged with nitrogen to remove oxygen in the apparatus. After filling the compartments of apparatus with nitrogen, the system pressure was increased up to 2.5 MPa at the experimental temperature for the leak test. Next, carbon dioxide was introduced into the cell to obtain the desired partial pressure. For easy sampling of the liquid phase, nitrogen was used to maintain the system pressure above atmospheric pressure when the partial pressure of  $CO_2$  is below atmospheric. Equilibrium was assumed when the system pressure and vapor-phase composition remained stable for, at least, 10 hours. It takes more than 24 hours to reach complete equilibrium. The analysis of the liquid samples was carried out by the titration method similar to that of Shen and Li [3]. The amount of water in the vapor phase was determined by Raoult's law. The partial pressure of CO<sub>2</sub> was directly calculated from the total system pressure, vapor-phase composition, and the partial pressure of water. Potassium carbonate, 1,2-propanediol, and propylene carbonate were assumed to be nonvolatile with negligible effect on the partial pressure of  $CO_2$ .

### 2.2. Materials

Potassium carbonate, 1,2-propanediol, and propylene carbonate were purchased from Sigma-Aldrich Chemical Co. Potassium carbonate was in anhydrous form with a minimum purity of 99.5 mol%. Water distilled in the laboratory was used. The carbon dioxide and nitrogen gases were of commercial grade with a minimum purity of 99.5 mol%.

#### 3. RESULTS AND DISCUSSION

Since the reliability of the equilibrium apparatus and experimental procedure has already been verified in our previous study [11], test measurements were not performed. In the present work, the solubilities of

 $CO_2$  in 5 mass %  $K_2CO_3$ -15 mass % 1,2-propanediol and 5 mass %  $K_2CO_3$ -30 mass % 1,2-propanediol aqueous solutions were measured at 298.2 and 323.2 K. The results are shown in Table I and plotted in Figs. 1 and 2 along with the solubilities in a 5 mass %  $K_2CO_3$  aqueous solution. The  $CO_2$  solubilities were represented by the loading, i.e., the mol of  $CO_2$  absorbed per mol of  $K_2CO_3$ . As shown in Figs. 1 and 2, the  $CO_2$  solubility increases with the partial pressure of  $CO_2$  and decreases with the solution temperature. The  $CO_2$  loading decreased gradually with an increase in the amount of 1,2-propanediol at constant temperature and pressure. The

Mixture	Т (К)	P <sub>CO2</sub> (kPa)	loading (mol of $CO_2$ /mol of $K_2CO_3$ )
5 mass % K <sub>2</sub> CO <sub>3</sub> -15 mass % 1,2-propanediol	298.2	6.16	0.774
		12.70	0.840
		29.97	0.810
		31.02	0.881
		133.0	1.049
		420.4	1.163
		854.0	1.424
		1283	1.579
	323.2	6.50	0.694
		19.51	0.782
		41.90	0.825
		42.11	0.832
		131.8	0.944
		472.3	1.053
		1180	1.285
5 mass % K <sub>2</sub> CO <sub>3</sub> -30 mass % 1,2-propanediol	298.2	6.31	0.730
		17.36	0.765
		45.61	0.849
		129.0	0.920
		428.1	1.075
		1053	1.313
		1346	1.442
	323.2	3.19	0.585
		20.25	0.708
		47.15	0.815
		127.6	0.888
		470.9	1.011
		1306	1.203

 Table I.
 Measured Solubility of Carbon Dioxide in Aqueous K2CO3-1,2-Propanediol Solutions

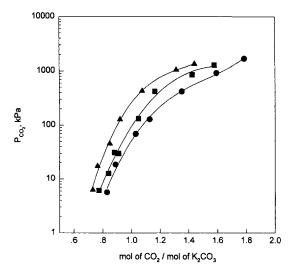


Fig. 1. Solubilities of carbon dioxide in aqueous 5 mass%  $K_2CO_3$ -1,2-propanediol solutions at 298.2 K: ( $\bullet$ ) 5 mass%  $K_2CO_3$ ; ( $\bullet$ ) 5 mass%  $K_2CO_3$ -15 mass% 1,2-propanediol; ( $\bullet$ ) 5 mass%  $K_2CO_3$ -30 mass% 1,2-propanediol.

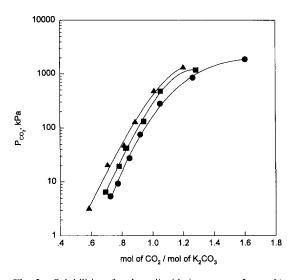


Fig. 2. Solubilities of carbon dioxide in aqueous 5 mass%  $K_2CO_3$ -1,2-propanediol solutions at 323.2 K: (•) 5 mass%  $K_2CO_3$ ; (•) 5 mass%  $K_2CO_3$ -15 mass% 1,2-propanediol; (•) 5 mass%  $K_2CO_3$ -30 mass% 1,2-propanediol.

solubility of CO<sub>2</sub> in 5 mass %  $K_2CO_3$ -7.5 mass % propylene carbonate and 5 mass %  $K_2CO_3$ -15 mass % propylene carbonate aqueous solutions was also measured at 298.2 and 323.2 K in order to examine the absorption efficiency of propylene carbonate. These data are reported in Table II and graphically compared with the results for a 5 mass %  $K_2CO_3$  aqueous solution in Figs. 3 and 4. The CO<sub>2</sub> solubilities increase as the mass % of propylene carbonate increases below atmospheric pressure (100 kPa) at 298.2 and 323.2 K, while, above 100 kPa, the CO<sub>2</sub> solubilities decrease with

T  $P_{\rm CO_2}$ (kPa) loading (mol of  $CO_2/mol$  of  $K_2CO_3$ ) Mixture (K) 5 mass % K<sub>2</sub>CO<sub>3</sub>-7.5 mass % 298.2 7.57 0.881 propylene carbonate 0.979 31.24 87.36 1.097 31.02 0.881 325.4 1.244 759.5 1.388 1627 1.651 323.2 0.747 5.41 16.22 0.845 55.98 0.936 153.4 1.017 670.4 1.178 1544 1.326 5 mass % K<sub>2</sub>CO<sub>3</sub>-15 mass % 298.2 6.61 0.928 propylene carbonate 0.971 13.38 38.98 1.076 1.202 418.3 430.7 1.225 1002 1.370 1031 1.403 1609 1.640 2000 1.800 323.2 0.783 6.38 13.36 0.874 50.00 0.971 192.3 1.027 760.3 1.153 1008 1.223 1838 1.358

 Table II.
 Measured Solubility of Carbon Dioxide in Aqueous K2CO3-Propylene Carbonate

 Solutions
 Solutions

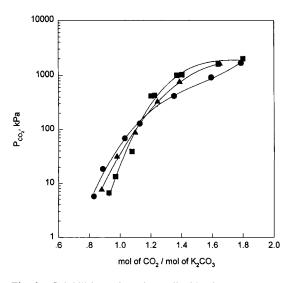


Fig. 3. Solubilities of carbon dioxide in aqueous 5 mass %  $K_2CO_3$ -propylene carbonate solutions at 298.2 K: (•) 5 mass %  $K_2CO_3$ ; (•) 5 mass %  $K_2CO_3$ -7.5 mass % propylene carbonate; (•) 5 mass %  $K_2CO_3$ -15 mass % propylene carbonate.

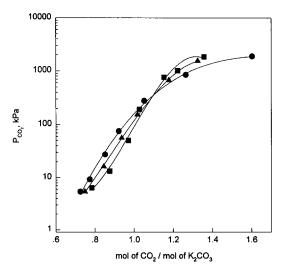


Fig. 4. Solubilities of carbon dioxide in aqueous 5 mass %  $K_2CO_3$ -propylene carbonate solutions at 323.2 K: (•) 5 mass %  $K_2CO_3$ ; (•) 5 mass %  $K_2CO_3$ -7.5 mass % propylene carbonate; (•) 5 mass %  $K_2CO_3$ -15 mass % propylene carbonate.

an increase in the propylene carbonate mass %. Due to a solubility limit, the experiment could not be extended to higher concentrations of propylene carbonate.

## 4. CONCLUSION

The equilibrium solubilities of  $CO_2$  in aqueous  $K_2CO_3$ -1,2propanediol and  $K_2CO_3$ -propylene carbonate solutions were measured at 298.2 and 323.2 K. The loadings of  $CO_2$  decrease with increasing temperature from 298.2 to 323.2 K. The addition of 1,2-propanediol to 5 mass%  $K_2CO_3$  solution lowers the solubility of  $CO_2$  at a constant temperature and pressure within the  $CO_2$  partial-pressure range of 5 kPa to 2 MPa. The  $CO_2$  solubility increases with the mass% of propylene carbonate below 100 kPa, while it decreases above 100 kPa at constant temperature and pressure.

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#### REFERENCES

- 1. A. L. Shrier and P. V. Danckwerts, Chem. Eng. Sci. 8:415 (1969).
- 2. P. H. M. Feron, A. E. Jansen, and R. Klaasen, Energy Convers. Mgmt. 33:421 (1992).
- 3. K. P. Shen and M. H. Lee, J. Chem. Eng. Data 37:96 (1992).
- 4. F. Murrieta-Guevara, E. Robolledo-Libreros, and A. Trejo, *Fluid Phase Equil.* 95:163 (1994).
- 5. F. Murrieta-Guevara, E. Robolledo-Libreros, and A. Trejo, Fluid Phase Equil. 53:1 (1989).
- 6. F. Murrieta-Guevara, E. Robolledo-Libreros, and A. Trejo, *Fluid Phase Equil.* 44:105 (1988).
- 7. A. Henni and A. E. Mather, J. Chem. Eng. Data 40:493 (1995).
- 8. J. S. Tosh, J. H. Field, H. E. Benson, and W. P. Haynes, U.S. Bureau of Mines Rept. of Investigations, No. 5484 (1959).
- 9. J. S. Tosh, J. H. Field, H. E. Benson, and R. B. Anderson, U.S. Bureau of Mines Rept. of Investigations, No. 5622 (1960).
- 10. H. E. Benson, J. H. Field, and W. P. Haynes, Chem. Eng. Prog. 52:433 (1956).
- 11. S. B. Park, C. S. Shim, H. Lee, and K. H. Lee, Fluid Phase Equil. 134:141 (1997).